

Test of Redfield's model for oxygen-nutrient relationships using regression analysis¹

Saul Alvarez-Borrego

Instituto de Investigaciones Oceanologicas, Universidad Autonoma de Baja California, Ensenada, Mexico

Donald Guthrie

Department of Statistics, Oregon State University, Corvallis 97331

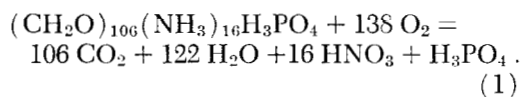
Charles H. Culberson and P. Kilho Park

School of Oceanography, Oregon State University

Abstract

Multiple regression analysis was applied to oxygen, phosphate, and nitrate data from stations in the Atlantic and Pacific Oceans. The 95% confidence intervals for $\Delta O_2 : \Delta PO_4$ and $\Delta O_2 : \Delta NO_3$ ratios were consistent with Redfield's model. Thus, the variation of O_2-PO_4 and O_2-NO_3 slopes with depth, latitude, and time is due to mixing between different water types with different preformed portions of oxygen, phosphate, and nitrate.

Redfield (1934, 1942; Redfield et al. 1963) proposed a relation between the concentrations of dissolved oxygen, carbon dioxide, nitrate, and phosphate in seawater based on the average chemical composition of plankton (Fleming 1941). This relation predicts that the ratio of oxygen consumption to nutrient production by biological oxidation is constant and can be represented by the equation



$(CH_2O)_{106}(NH_3)_{16}H_3PO_4$ is a hypothetical organic molecule containing carbon, nitrogen, and phosphorus in the ratio in which they occur in plankton. Equation 1 predicts that the consumption of 276 oxygen atoms results in the production of 106 carbon atoms, 16 nitrogen atoms, and 1 phosphorus atom.

Theoretically, the best way to test Redfield's model is to plot oxygen consumption (apparent oxygen utilization: AOU) ver-

sus the increase in concentration of a nutrient arising from this biological oxidation; at present however, changes in nutrient concentrations due to biological oxidation cannot be calculated independently without the use of this model. The purpose of our work was to test Redfield's model for the O_2-PO_4 and O_2-NO_3 relationships by applying multiple regression analysis to field data.

Data sources

We used hydrographic data from the following cruises: YALOC-66 (Barstow et al. 1968), SCORPIO (Scripps Inst. Oceanogr. Data Rep. Ref. 69-15, Woods Hole Oceanogr. Inst. Data Rep. Ref. 69-56), SOUTHERN CROSS (Horibe 1970), and from GEOSECS intercalibration stations in the Atlantic (Spencer 1970) and Pacific (GOGO-I unpublished data). Station positions are shown in Fig. 1. Nutrient measurements during GOGO-I were made by a Technicon AutoAnalyzer with a precision of $\pm 1\%$ or better. Nutrient determinations on all other cruises were made by manual methods. The precision of nutrient analyses is not reported for YALOC-66 and SCORPIO expeditions. For the SOUTHERN CROSS cruise, the estimated precision was $\pm 4\%$ for nitrate and $\pm 3\%$ for phosphate (Horibe 1970).

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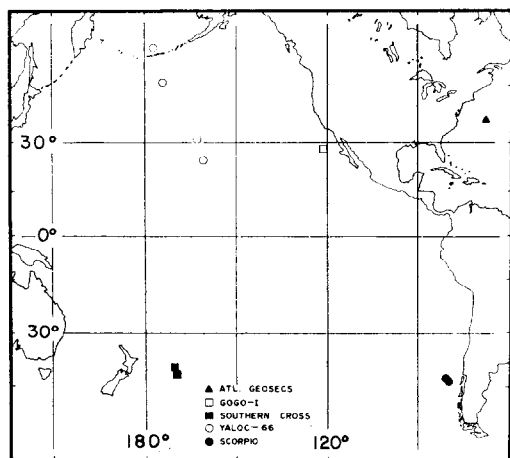


Fig. 1. Locations of the hydrographic stations used in this study.

Discussion

The regeneration of nitrate in seawater is more complicated than that of phosphate. Nitrogen is released from organic substances as ammonia and subsequently oxidized to nitrite, and then to nitrate (Redfield et al. 1963). Ammonia and nitrite are not ordinarily found in significant quantities below the photosynthetic zone in the deep sea, and we will assume that all nitrogen derived from biological oxidation is in the form of nitrate.

When O_2 is expressed in ml liter^{-1} , and PO_4 and NO_3 are in μM , the ratios proposed by Redfield et al. (1963) are $O_2 : PO_4 = -3.1$, $O_2 : NO_3 = -0.19$. From Redfield et al. (1963),

$$AOU = O_2' - O_2, \quad (2)$$

$$PO_4 = PO_{4(ox)} + PO_{4(p)}, \quad (3)$$

$$PO_{4(ox)} = (AOU)/3.1, \quad (4)$$

$$NO_3 = NO_{3(ox)} + NO_{3(p)}, \quad (5)$$

and

$$NO_{3(ox)} = (AOU)/0.19, \quad (6)$$

where O_2' is the calculated concentration of dissolved oxygen at saturation with a wet atmosphere at the potential temperature of the sample; $PO_{4(ox)}$ and $NO_{3(ox)}$ are the phosphate and nitrate released by biological oxidation; and $PO_{4(p)}$ and $NO_{3(p)}$ are the preformed phosphate and nitrate. Rearranging Eq. 2-6 yields

$$O_2 = -3.1 PO_4 + [O_2' + 3.1 PO_{4(p)}], \quad (7)$$

and

$$O_2 = -0.19 NO_3 + [O_2' + 0.19 NO_{3(p)}]. \quad (8)$$

From Eq. 7 and 8 we see that if Redfield's model is correct, any variation of the O_2 - PO_4 and O_2 - NO_3 slopes with location, depth, and time is due to mixing between water types with different values of preformed O_2 (O_2'), PO_4 , and NO_3 .

Test of Redfield's model by regression analysis—One way to test Redfield's model is by using regression analysis on field data. If we regress O_2 on PO_4 , temperature and salinity, the temperature or salinity terms may represent the conservative fraction of phosphate and oxygen, namely $O_2' + 3.1 PO_{4(p)}$, so that the PO_4 term represents only the nonconservative fractions. The same type of approach can be used for the O_2 - NO_3 relationship.

Ben-Yaakov (1971) applied regression analysis to ΣCO_2 , O_2 , total alkalinity, salinity, S , and temperature data. He showed that, when dealing with a water mass which results from the mixing of n water types, at least $n-1$ conservative parameters are needed in the regression equation.

We will first use the regression analysis to test Redfield's model for the $\Delta O_2 : \Delta PO_4$ ratio, and then apply the same procedure to the $\Delta O_2 : \Delta NO_3$ ratio. To test the hypothesis that the $\Delta O_2 : \Delta PO_4$ ratio is equal to -3.1 , the regression equation

$$O_2 = a_0 + a_1 PO_4 + a_2 \theta + O_{2(res)} \quad (9)$$

was applied to the data, where $O_{2(res)}$ are the O_2 residuals after regression of O_2 on PO_4 and potential temperature (θ); a_0 , a_1 , and a_2 are constant regression coefficients. a_1 equals $\Delta O_2 : \Delta PO_4$. Potential temperature is used to eliminate the effect of adiabatic heating; it is preferred to S because O_2' depends more on temperature than on S .

It may seem that to apply Eq. 9 to field data we must choose a portion of the water column where no more than two water types are mixed, since we only have one conservative variable in the equation. But by comparing Eq. 7 and 9 we see that the

Test of Redfield's model

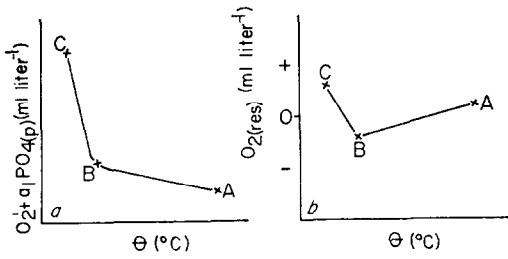


Fig. 2. $O_2' + a_1PO_{4(p)}$ versus θ —a; $O_{2(res)}$ versus θ —b, of a hypothetical station.

only condition necessary for the proper application of 9 is that the conservative quantity $O_2' + a_1PO_{4(p)}$ be a linear function of θ . That is

$$O_2' + a_1 PO_{4(p)} = a_0 + a_2\theta. \quad (10)$$

This means that Eq. 9 must be applied to data from a portion of the water column where a diagram of $O_2' + a_1PO_{4(p)}$ versus θ can detect only two-point mixing.

If Eq. 9 is applied to the proper portion of the water column, a plot of $O_{2(res)}$ versus θ should be completely random, because $O_{2(res)}$ should result from only the random errors in the measurements of O_2 , PO_4 , and θ . Thus, if we apply 9 to the whole water column and plot $O_{2(res)}$ versus θ , the pattern shown by the diagram, if any, will give us an indication of how to separate the water column into suitable portions.

Suppose we have data from the whole water column of a certain station, and it yields the $O_2' + a_1PO_{4(p)}$ versus θ diagram similar to the one shown in Fig. 2a where three water types, A, B, and C, have been detected. Since $O_2' + a_1PO_{4(p)}$ is not a linear function of θ , a plot of $O_{2(res)}$ versus θ would generate a diagram as shown in Fig. 2b. Each minimum and maximum in the $O_{2(res)}$ versus θ diagram represents a different water type. This procedure was applied to data from station HAH30 of YALOC-66 ($30^\circ55.4'N$, $162^\circ37.4'W$) (Bartow et al. 1968). This station was chosen because samples were taken from 49 different depths. Most published data contain no more than 30 observations per station. The number of observations is important because the standard errors of the

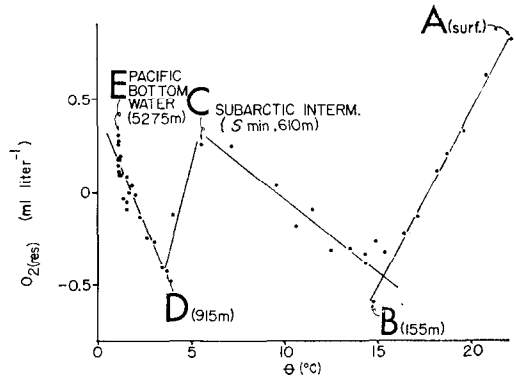


Fig. 3. $O_{2(res)}$ versus θ diagram for the whole water column of station HAH30 ($30^\circ55.4'N$, $162^\circ37.4'W$). A, B, C, D, and E denote water types.

regression coefficients decrease as the degrees of freedom increase. Multiple linear regression analysis is a least square fit to the given data. The fitting was accomplished by a computer program (SIPS: Oregon State Univ. Dep. Statistics). For each coefficient of the following regression equations, 95% confidence intervals are given.

The results are as follows. Regressing O_2 on PO_4 and θ for the whole water column, 0–5,275 m, we find the regression equations

with PO_4 only:

$$O_2 = (5.79 \pm 0.36) - (1.27 \pm 0.17)PO_4; \quad (11)$$

with PO_4 and θ :

$$O_2 = (10.65 \pm 0.78) - (0.27 \pm 0.04)\theta - (2.85 \pm 0.26)PO_4. \quad (12)$$

Equation 12 has a coefficient of determination $R^2 = 0.969$.

Figure 3 shows a definite dependency of $O_{2(res)}$ on θ . Since the O_2' versus θ diagram is a smooth curve (Fig. 4), the pattern shown in Fig. 3 is due to differences in $PO_{4(p)}$ between different water types. In Fig. 3, A is surface water, C is Subarctic Intermediate Water with a salinity minimum, D coincides almost with the O_2 minimum, E is Pacific Bottom Water. The θ -S diagram (Fig. 5) does not show B and D distinctly, but suggests their presence be-

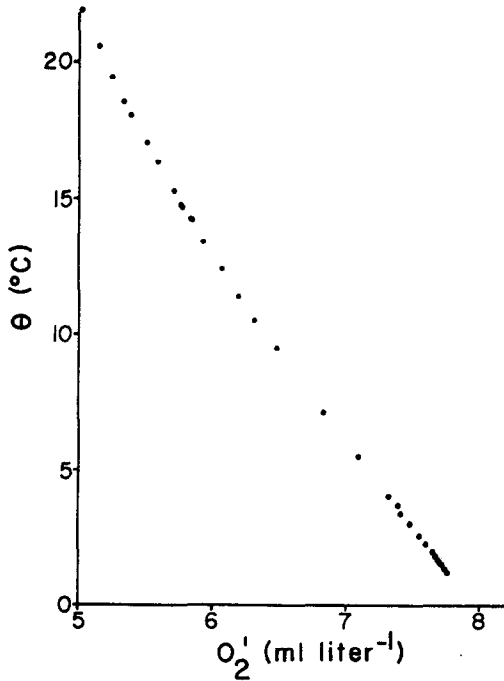


Fig. 4. O_2' versus θ diagram for the whole water column of station HAH30.

cause the θ -S diagram is not linear in their vicinity. For Antarctic Intermediate Water, Reid (1965) chose the surface of thermoclinic anomaly (δ_t) equal to 80 cl ton⁻¹, $\sigma_t = 27.28$. Water D (Fig. 3) has a σ_t of 27.32.

The confidence interval for the PO_4 re-

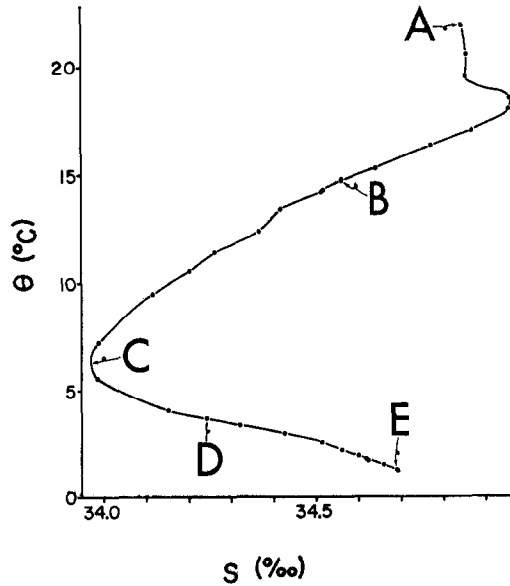


Fig. 5. θ -S diagram for station HAH30 (30° 55.4'N, 162°37.4'W). A, B, C, D, and E denote same water types shown in Fig. 3.

gression coefficient, $-(2.85 \pm 0.26)$, in Eq. 12 is consistent with Redfield's model. This agreement is fortuitous since the plot of $O_{2(res)}$ versus θ (Fig. 3) is not random.

The data from HAH30 was separated into three sets: A to B, B to C, and D to E. Between C and D (Fig. 3) there is only one data point so no regression was applied to that portion of the water column.

Table 1. Regression equations of O_2 on PO_4 and θ for different portions of the water column of station HAH30.

Portion of the water column	Regression equations (showing 95% confidence intervals)	Equation number
A-B (0-155 m)	with PO_4 only: $O_2 = (5.54 \pm 0.15) - (1.12 \pm 0.80)PO_4$	13
	with PO_4 and θ : $O_2 = (7.08 \pm 0.60) - (0.07 \pm 0.03)\theta - (2.50 \pm 0.64)PO_4$	14
B-C (155-610 m)	with PO_4 only: $O_2 = (5.71 \pm 0.24) - (1.20 \pm 0.20)PO_4$	15
	with PO_4 and θ : $O_2 = (10.91 \pm 1.84) - (0.32 \pm 0.12)\theta - (2.71 \pm 0.54)PO_4$	16
D-E (915-5,275)	with PO_4 only: $O_2 = (14.18 \pm 0.70) - (4.3 \pm 0.26)PO_4$	17
	with PO_4 and θ : $O_2 = (11.27 \pm 0.78) - (0.49 \pm 0.12)\theta - (2.93 \pm 0.36)PO_4$	18

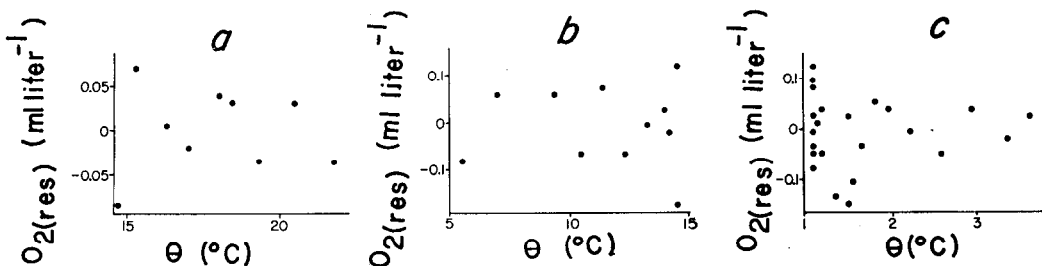


Fig. 6. $O_{2(res)}$ versus θ diagrams for portions of the water column. a—0 to 155 m; b—155 to 610 m; c—915 to 5,275 m, station HAH30.

The results of the regressions for this station are shown in Table 1.

Equations 14, 16, and 18 (given in Table 1) have coefficients of determination, R^2 , equal to 0.915, 0.988, and 0.996.

$O_{2(res)}$ versus θ diagrams for these three sets of data show no particular trend (Fig. 6). This indicates that $O_{2(res)}$ results only from random errors in the O_2 , PO_4 , and θ data, and that Eq. 14, 16, and 18 properly describe the data.

The PO_4 regression coefficients of Eq. 13, 15, and 17 (Table 1) are the least squares slopes we obtained by plotting O_2 versus PO_4 directly. Before θ is added to the regression equations, the PO_4 regression coefficients for A-B and B-C are smaller than the value predicted by Redfield's model, and those for D-E greater. After adding θ to the equations, the phosphate regression coefficients approach the predicted value, -3.1 , more closely.

To test the hypothesis that the $\Delta O_2 : \Delta NO_3$ ratio equals -0.19 , the regression equation

$$O_2 = b_0 + b_1 NO_3 + b_2 \theta + O_{2(res')} \quad (19)$$

was applied to the data, where $O_{2(res')}$ are the O_2 residuals after regression of O_2 on NO_3 and θ ; b_0 , b_1 , and b_2 are constant regression coefficients, and b_1 equals $\Delta O_2 : \Delta NO_3$.

Applying Eq. 19 to data from HAH30 (no NO_3 data for upper 35 m) we obtained the following results

with NO_3 only:

$$O_2 = (5.71 \pm 0.42) - (0.889 \pm 0.014) NO_3; \quad (20)$$

with NO_3 and θ :

$$O_2 = (10.98 \pm 1.08) - (0.33 \pm 0.12) \theta - (0.21 \pm 0.02) NO_3. \quad (21)$$

Equation 21 has a coefficient of determination $R^2 = 0.953$.

Figure 7 shows a definite dependency of $O_{2(res')}$ on θ . It also shows very clearly the Subarctic Intermediate Water and water type D shown in Fig. 3. Below 3,725 m values for $O_{2(res')}$ vary randomly. The data points scatter more in Fig. 7 than in Fig. 3 because NO_3 data are not as precise as PO_4 data from this station. During YALOC-66, PO_4 samples were analyzed immediately while NO_3 samples were frozen and analyzed ashore (Barstow et al. 1968).

The confidence interval for the NO_3 regression coefficient of Eq. 22 (Table 2), -0.19 to -0.23 , is consistent with Redfield's model—a fortuitous agreement since the plot of $O_{2(res')}$ versus θ (Fig. 7) is not ran-

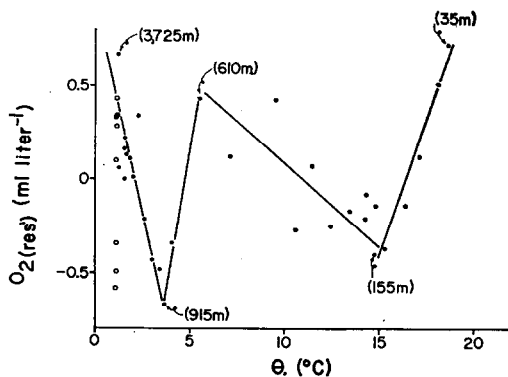


Fig. 7. $O_{2(res')}$ versus θ diagram for the whole water column of station HAH30. Open circles represent data from below 3,725 m.

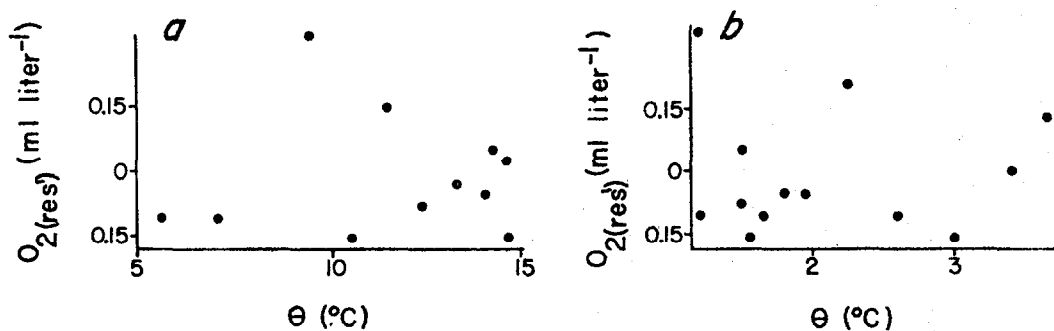


Fig. 8. $O_{2(res)}$ versus θ diagrams for portions of the water column. a—155 to 610 m; b—915 to 3,725 m, station HAH30.

dom. To test Redfield's model we divided the NO_3 data into two sets, 155 to 610 m and 915 to 3,725 m. The regression for the 35–155-m depth range was not significant as there are only six data points for that portion of the water column (Fig. 7). The results of the regressions for this station are shown as Eq. 22–25 in Table 2. Equations 23 and 25 have coefficients of determination, R^2 , equal to 0.966 and 0.978.

The $O_{2(res)}$ versus θ diagrams for these two sets of data are random (Fig. 8). This indicates that $O_{2(res)}$ result only from random errors of O_2 , NO_3 , and θ data, and that Eq. 23 and 25 properly describe the data. The NO_3 regression coefficients of 23 and 25 are consistent with Redfield's model.

Equations 9 and 19 were applied to data from other stations to study the effect of geographic location. The results are shown in Tables 3 and 4. There are no NO_3 data

for station HAH52 (Barstow et al. 1968). For the Atlantic GEOSECS station, the Scripps' O_2 data were used (Spencer 1970). Regression equations for those without the θ term are given in Tables 3 and 4 for comparison of O_2-PO_4 and O_2-NO_3 slopes before and after the mixing effect is extracted.

The precision of the regression coefficients depends on the random errors of the O_2 , PO_4 , NO_3 , and θ measurements, the range of these properties, and the degrees of freedom of the residuals. Poor precision does not necessarily mean bad field data. Tables 3 and 4 show that in some cases the residuals had only 3 df: with 3 df the value for $t_{(0.025)}$ is 3.18. Some regions of the water column were not tabulated in Tables 3 and 4, because either the O_2 , PO_4 , and NO_3 ranges were too small or there were not enough data points to apply the regression analysis.

Table 2. Regression equations of O_2 on NO_3 and θ for different portions of the water column of station HAH30.

Portion of the water column	Regression equations (showing 95% confidence intervals)	Equation number
155-610 m	with NO_3 only: $O_2 = (5.57 \pm 0.22) - (0.081 \pm 0.014)NO_3$	22
	with NO_3 and θ : $O_2 = (9.56 \pm 2.82) - (0.26 \pm 0.18)\theta - (0.16 \pm 0.06)NO_3$	23
915-3,725 m	with NO_3 only: $O_2 = (16.76 \pm 4.56) - (0.364 \pm 0.110)NO_3$	24
	with NO_3 and θ : $O_2 = (9.36 \pm 2.26) - (0.87 \pm 0.20)\theta - (0.14 \pm 0.06)NO_3$	25

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Table 3. Regression equations of O_2 on PO_4 and θ , on PO_4 and S , on NO_3 and θ , and on NO_3 and S . The confidence intervals are at the 95% confidence level. Stations HAH52, AAH2, and SCORPIO 71 and 72.

Station	Depth range (meters)	Regression equations (showing 95% confidence intervals)	R^2	$n-p-1$
HAH52 (45° 52.8'N, 174° 2.3'W)	125-405	with PO_4 only: $O_2 = (9.90 \pm 0.39) - (2.78 \pm 0.20)PO_4$ with PO_4 & θ : $O_2 = (14.02 \pm 3.91) - (3.49 \pm 0.58)PO_4 - (0.50 \pm 0.48)\theta$	0.999	4 3
	405-1765	with PO_4 only: $O_2 = (12.59 \pm 2.02) - (3.75 \pm 0.66)PO_4$ with PO_4 & θ : $O_2 = (13.24 \pm 7.67) - (3.92 \pm 1.95)PO_4 - (0.05 \pm 0.55)\theta$	0.978 0.979	5 4
AAH2 (52° 56.1'N, 179° 55'W)	75-300	with PO_4 only: $O_2 = (22.87 \pm 0.90) - (7.05 \pm 0.35)PO_4$ with PO_4 & S : $O_2 = (186 \pm 96) - (2.9 \pm 2.6)PO_4 - (5.2 \pm 3.1)S$	0.999	6 5
	360-1020	with PO_4 only: $O_2 = (24.4 \pm 6.4) - (7.4 \pm 2.0)PO_4$ with PO_4 & S : $O_2 = (74.4 \pm 23.5) - (3.3 \pm 2.2)PO_4 - (1.85 \pm 0.86)S$	0.985	7 6
	1215-3200	with PO_4 only: $O_2 = (20.33 \pm 2.04) - (6.15 \pm 0.66)PO_4$ with PO_4 & S : $O_2 = -(74.9 \pm 50.8) - (4.21 \pm 1.14)PO_4 + (2.58 \pm 1.28)S$	0.987	11 10
	515-3500	with NO_3 only: $O_2 = (14.03 \pm 2.06) - (0.297 \pm 0.046)NO_3$ with NO_3 & S : $O_2 = -(40.2 \pm 36.7) - (0.224 \pm 0.060)NO_3 + (1.5 \pm 1.0)S$	0.961	12 11
SCORPIO 71 & 72 (off Chile)	90-865	with PO_4 only: $O_2 = (6.88 \pm 1.06) - (0.82 \pm 0.62)PO_4$ with PO_4 & θ : $O_2 = (13.80 \pm 0.70) - (3.12 \pm 0.26)PO_4 - (0.45 \pm 0.04)\theta$	0.962	24 23
	80-840	with NO_3 only: $O_2 = (6.49 \pm 0.92) - (0.04 \pm 0.04)NO_3$ with NO_3 & θ : $O_2 = (15.91 \pm 1.48) - (0.26 \pm 0.04)NO_3 - (0.62 \pm 0.10)\theta$	0.902	24 23

* $n-p-1$ are the residual degrees of freedom, n is the number of observations and p is the number of independent variables already in the regression equation.

Table 4. Regression equations of O_2 on PO_4 and θ , and on NO_3 and θ . The confidence intervals are at the 95% confidence level. North Pacific and North Atlantic GEOSECS intercalibration stations.

Station	Depth range (meters)	Regression equations (showing 95% confidence intervals)	R^2	$n-p-1$
GOGO I (GEOSECS) (28° 29'N, 121° 38'W) (off Baja California)	260-800	with PO_4 only: $O_2 = 7.60 \pm 0.57) - (2.22 \pm 0.21)PO_4$ with PO_4 & θ : $O_2 = (10.78 \pm 1.20) - (2.82 \pm 0.23)PO_4 - (0.23 \pm 0.07)\theta$	0.999	6 5
	1200-4200	with PO_4 only: $O_2 = (12.81 \pm 0.44) - (3.61 \pm 0.16)PO_4$ with PO_4 & θ : $O_2 = (11.50 \pm 1.54) - (3.05 \pm 0.66)PO_4 - (0.19 \pm 0.21)\theta$	0.994	16 15
	905-2005	with NO_3 only: $O_2 = (17.17 \pm 4.16) - (0.38 \pm 0.10)NO_3$ with NO_3 & θ : $O_2 = (9.77 \pm 3.36) - (0.18 \pm 0.08)NO_3 - (0.36 \pm 0.14)\theta$	0.997	5 4
	2005-4200	with NO_3 only: $O_2 = (17.91 \pm 2.64) - (0.39 \pm 0.07)NO_3$ with NO_3 & θ : $O_2 = (8.90 \pm 2.4) - (0.12 \pm 0.07)NO_3 - (1.19 \pm 0.28)\theta$	0.992	12 11
ATLANTIC STATION (GEOSECS) (35° 46.0'N, 67° 58.0'W)	430-860	with PO_4 only: $O_2 = (5.17 \pm 0.11) - (1.58 \pm 0.20)PO_4$ with PO_4 & θ : $O_2 = (8.52 \pm 3.84) - (2.72 \pm 1.31)PO_4 - (0.18 \pm 0.17)\theta$	0.998	4 3
	860-1840	with PO_4 only: $O_2 = (9.11 \pm 6.67) - (3.18 \pm 5.29)PO_4$ with PO_4 & θ : $O_2 = (10.49 \pm 0.74) - (2.62 \pm 0.53)PO_4 - (0.35 \pm 0.02)\theta$	0.993	8 7
	150-580	with NO_3 only: $O_2 = (4.97 \pm 0.29) - (0.041 \pm 0.059)NO_3$ with NO_3 & θ : $O_2 = (11.09 \pm 3.44) - (0.18 \pm 0.08)NO_3 - (0.31 \pm 0.17)\theta$	0.905	5 4
	860-1840	with NO_3 only: $O_2 = (12.18 \pm 5.75) - (0.36 \pm 0.28)NO_3$ with NO_3 & θ : $O_2 = (10.82 \pm 0.67) - (0.20 \pm 0.04)NO_3 - (0.30 \pm 0.03)\theta$	0.995	8 7
	1840-4915	with NO_3 only: $O_2 = (7.43 \pm 1.12) - (0.07 \pm 0.06)NO_3$ with NO_3 & θ : $O_2 = (9.26 \pm 1.54) - (0.16 \pm 0.08)NO_3 - (0.11 \pm 0.08)\theta$	0.571	14 13

* $n-p-1$ are the residual degrees of freedom, n is the number of observations and p is the number of independent variables already in the regression equation.

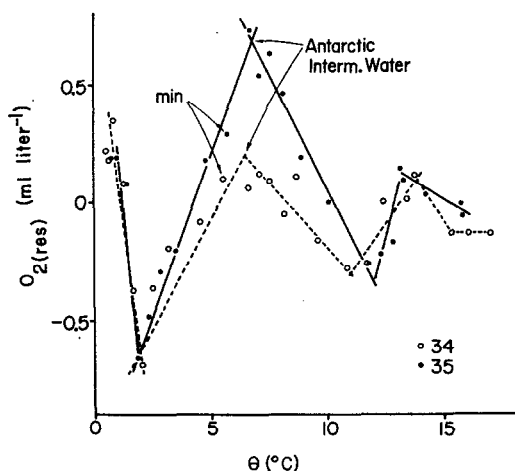


Fig. 9. $O_{2(res)}$ versus θ diagrams for the whole water column of stations 34 and 35 of the SOUTHERN CROSS cruise ($39^{\circ}59.5'S$, $170^{\circ}03.2'W$ and $42^{\circ}01.2'S$, $170^{\circ}01.8'W$).

For station AAH2, in the southeastern Bering Sea, the presence of a temperature minimum and maximum in the upper 400 m (Alvarez-Borrego et al. 1972) made S a better parameter than θ for the regressions; a higher coefficient of determination was obtained using S instead of θ as the independent variable. At HAH52 the temperature minimum and maximum are also present but θ was used in the regression with satisfactory results (Table 3). In the Atlantic and South Pacific Oceans, changes of O_2 , PO_4 , and NO_3 are not as great as in the North Pacific Ocean. When changes in these properties are small, random errors of the determinations are large in percentage. SCORPIO stations 71 and 72 are geographically close, $43^{\circ}14.7'S$, $80^{\circ}02.0'W$, and $43^{\circ}19.0'S$, $79^{\circ}01.5'W$, and were treated together to have more degrees of freedom for the regression.

With few exceptions, the results are consistent with Redfield's model (Tables 3 and 4). For SCORPIO stations 71 and 72 the PO_4 regression coefficient is slightly higher than the value predicted by Redfield's model. The adjustment of the NO_3 regression coefficient after θ was added to the equation was in the right direction, but

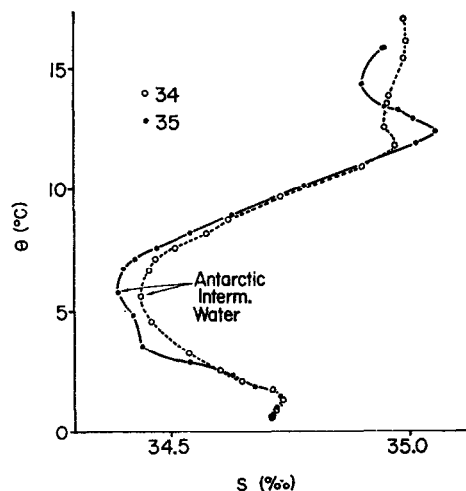


Fig. 10. θ - S diagrams for stations 34 and 35 of the SOUTHERN CROSS cruise.

it went too far (Table 3). In some cases the PO_4 and NO_3 regression coefficients were not significantly different from zero before θ was added to the equations, but they became consistent with Redfield's model when it was added (Tables 3 and 4).

The confidence interval for the PO_4 regression coefficient after θ is added to the equation is -4.21 ± 1.14 (Table 3) at station AAH2 (1,215–3,200 m). Alvarez-Borrego et al. (1972) applied regression analysis to the region of the water column where the θ - S diagram is straight (1,300–3,600 m). They treated data from stations AAH2 and AAH9 (also in the southeastern Bering Sea) together and obtained a PO_4 regression coefficient of -3.4 ± 1.0 . The confidence interval in this case is larger because we have fewer degrees of freedom. Alvarez-Borrego et al. (1972) calculated $PO_{4(p)}$ using Redfield's model, plotted it versus θ for the region of the water column where they applied the regression, and found a significant, although not very pronounced, departure from linearity. On this basis they indicated that their application of regression analysis to test Redfield's model was a first approximation. The $O_{2(res)}$ - θ diagram for the whole water column of station AAH2 does not detect the presence of a third water type for the depth range 1,215–

Test of Redfield's model

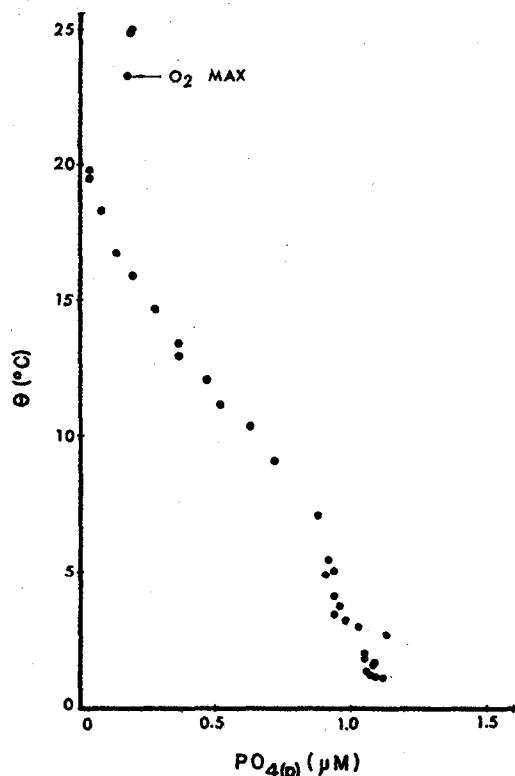


Fig. 11. θ versus $PO_{4(p)}$ diagram for station HAH22 ($24^{\circ}30.6'N$, $161^{\circ}30.0'W$).

3,200 m (not shown). The $O_{2(res)}-\theta$ diagram can clearly detect different water types only when abrupt inflections in the $O_2' + a_1PO_{4(p)}$ versus θ diagram exist. The confidence intervals obtained by Alvarez-Borrego et al. (1972) and here are consistent with Redfield's model.

Proportion of water types—We used data from the SOUTHERN CROSS cruise (Horibe 1970) to test Redfield's model in the South Pacific Ocean. The ranges for O_2 , PO_4 , and θ are smaller than in the North Pacific Ocean and we did not obtain a significant regression when applying our method to data from one station. Because of this, we applied Eq. 9 to data from two stations simultaneously. The $O_{2(res)}-\theta$ diagram (Fig. 9) shows that the proportions of the different water types are different at each station. We cannot represent data from both stations with the same set of re-

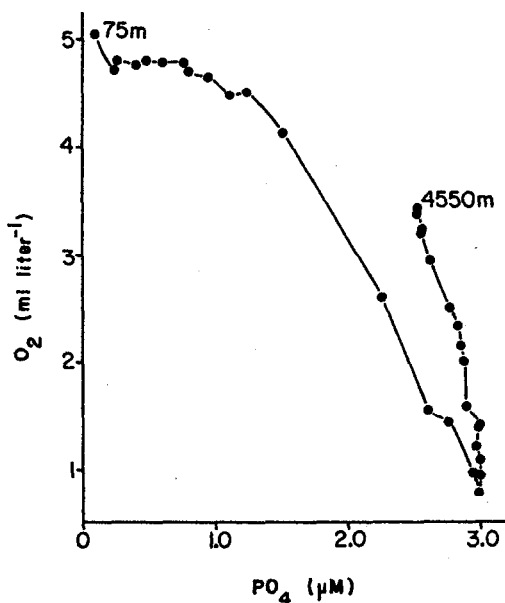


Fig. 12. O_2 versus PO_4 diagram for station HAH22.

gression equations. Figure 9 shows that when Eq. 9 has been applied to data from two geographically close stations, the $O_{2(res)}-\theta$ diagram may be used to indicate which station has a higher proportion of a certain water type. The $O_{2(res)}-\theta$ diagram (Fig. 9) and the θ -S diagram (Fig. 10) show that station 35 has a higher proportion of Antarctic Intermediate Water (station 35 is farther south than 34). The $O_{2(res)}-\theta$ diagram does not give any differentiation for SCORPIO stations 71 and 72 (not shown).

Estimation of mixing—Station HAH22 has an almost linear $PO_{4(p)}-\theta$ diagram for the region of the water column (75–4,550 m) below the near-surface O_2 maximum (Fig. 11). Its $O_2'-\theta$ diagram is similar to that for HAH30 (Fig. 4). This allows us to illustrate the extraction of the mixing effect by adding a conservative property, such as θ , to the regression equation. The O_2-PO_4 diagram for station HAH22 (Fig. 12) has a hooklike shape; if this is due to variation in the preformed quantities, θ should extract the mixing effect and leave a linear relationship between O_2 and PO_4 .

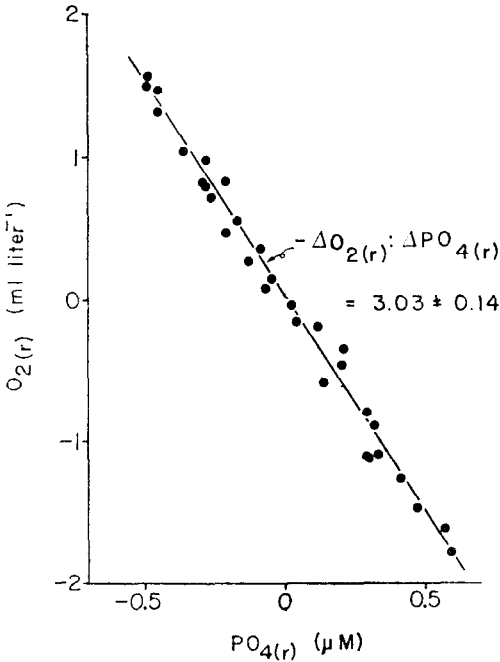


Fig. 13. $O_{2(r)}$ versus $PO_{4(r)}$ diagram for station HAH22.

This is only a first approximation because the O_2' - θ and $PO_{4(r)}$ - θ diagrams are not completely linear.

When O_2 is regressed on PO_4 and θ , the PO_4 term represents the regression of the residuals of O_2 after regression on θ . The residuals of PO_4 which resulted from a simple linear regression on θ are then fitted with $O_{2(r)}$. When we do the regression in a stepwise manner, adding θ first, we have

$$O_2 = c_0 + c_1\theta + O_{2(r)}. \quad (26)$$

Implicitly and simultaneously

$$PO_4 = d_0 + d_1\theta + PO_{4(r)}, \quad (27)$$

where c_0 , c_1 , d_0 , and d_1 are constant regression coefficients and $O_{2(r)}$ and $PO_{4(r)}$ are the O_2 and PO_4 residuals after regression on θ .

Adding PO_4 to regression Eq. 26, we regress $O_{2(r)}$ on $PO_{4(r)}$,

$$O_{2(r)} = f_0 + a_1 PO_{4(r)} + O_{2(res)}, \quad (28)$$

where f_0 and a_1 are constant regression coefficients and $O_{2(res)}$ is defined in Eq. 9.

Substituting the value of $PO_{4(r)}$ from 27 into 28 we have

$$O_{2(r)} = (f_0 - a_1 d_0) + a_1 PO_4 - a_1 d_1 \theta + O_{2(res)}, \quad (29)$$

and substituting 29 into 26 we have

$$O_2 = (c_0 + f_0 - a_1 d_0) + a_1 PO_4 + (c_1 - a_1 d_1)\theta + O_{2(res)}. \quad (30)$$

The terms $(C_0 + f_0 - a_1 d_0)$ and $(c_1 - a_1 d_1)$ are constants and can be represented by a_0 and a_2 . Therefore, Eq. 30 is the same as 9. The PO_4 regression coefficient of Eq. 9, a_1 , is the slope of the $O_{2(r)}$ versus $PO_{4(r)}$ diagram.

For station HAH22 the O_2 - PO_4 , O_2 - θ , and PO_4 - θ correlation coefficients are -0.91 , 0.75 , and -0.95 . Applying Eq. 26 and 27 we have

$$O_2 = (1.68 \pm 0.56) + (0.18 \pm 0.06)\theta, \quad (31)$$

and

$$PO_4 = (3.19 \pm 0.18) - (0.16 \pm 0.02)\theta. \quad (32)$$

Figure 13 shows the $O_{2(r)}$ versus $PO_{4(r)}$ diagram. The hooklike shape shown in Fig. 12 has disappeared after θ has extracted the mixing effect. The $O_{2(r)}$ - $PO_{4(r)}$ correlation coefficient is -0.99 and the confidence interval for the $O_{2(r)}$ - $PO_{4(r)}$ slope is -3.03 ± 0.14 , which is consistent with Redfield's model. In Fig. 13 the data points are not sequential with depth: points at one end are not necessarily near-surface points, and points at the other end are not necessarily deep points. Data points at the lower end of the $O_{2(r)}$ - $PO_{4(r)}$ diagram correspond to the O_2 minimum zone.

$O_{2(r)}$ and $PO_{4(r)}$ should not be regarded as nonconservative fractions of O_2 and PO_4 . $O_{2(r)}$ and $PO_{4(r)}$ values by definition become zero when added. For this station the calculated ranges for AOU and $PO_{4(ox)}$ are 0.16 to 6.40 ml liter $^{-1}$ and 0.05 to 2.05 μ M. The ranges for $O_{2(r)}$ and $PO_{4(r)}$ are only about half the ranges for AOU and $PO_{4(ox)}$ (Fig. 13) because AOU and $PO_{4(ox)}$ are partially correlated with θ . Thus, when we make the stepwise regression adding θ first as shown in Eq. 26, the θ term contains information about $O_2' +$

Test of Redfield's model

3.1 $\text{PO}_{4(\text{P})}$, AOU, and $\text{PO}_{4(\text{OX})}$. The complete regression equation for HAH22 (75–4,550 m) is

$$\text{O}_2 = (11.33 \pm 0.45) - (0.31 \pm 0.02)\theta - (3.03 \pm 0.14)\text{PO}_4 \quad (33)$$

with a coefficient of determination $R^2 = 0.994$.

In summary, our multiple regression analysis gave results consistent with values predicted by Redfield's model for ΔO_2 : ΔPO_4 and ΔO_2 : ΔNO_3 ratios. Diagrams of O_2 residuals after regression of O_2 on θ and PO_4 on θ or NO_3 can be used to detect water types, some of which are not clearly shown by θ -S diagrams. Qualitative studies on the proportions of water types at different stations can also be done using the O_2 residuals versus θ diagram.

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